



Legend

Site Boundary

Breach 10

Velocity (m/s)

<= 0.25

0.25 - 0.50

0.50 - 1.00

1.00 - 1.50

1.50 - 2.00












2.00 - 2.50

> 2.50

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REV:	DESCRIPTION:	BY:	DATE:
STATUS: FOR INFORMATION			
CLIENT: RWE			
SITE: Peartree Hill Solar Farm			
TITLE: Monk's Dyke Breach 10 100yr + 17% Maximum Velocity			
 <small>Transport Planning Flood Risk & Hydrology Infrastructure & Drainage 33 Colston Avenue Bristol BS1 4JA 0117 2441 970 E: hello@calibro-consultants.com W: www.calibro-consultants.com</small>			
SCALE AT A3: 1:14,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-128	REVISION: -	



Legend

- Site Boundary 
- Breach 11 
- Depth (m)
- 0 - 0.1 
 - 0.1 - 0.3 
 - 0.3 - 0.5 
 - 0.5 - 0.7 
 - 0.7 - 0.9 
 - 0.9 - 1.1 
 - 1.1 - 1.5 
 - 1.5 - 1.8 
 - >1.8 

-	FIRST ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
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SITE:
Peartree Hill Solar Farm

TITLE:
Monk's Dyke Breach 11
100yr + 17% Maximum Depth












SCALE AT A3: 1:14,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
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Legend

- Site Boundary 
- Breach 11 
- Velocity (m/s)
- ≤ 0.25 
 - 0.25 - 0.50 
 - 0.50 - 1.00 
 - 1.00 - 1.50 
 - 1.50 - 2.00 
 - 2.00 - 2.50 
 - > 2.50 

-	FIRST ISSUE	CF	23.04.2024
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STATUS: FOR INFORMATION

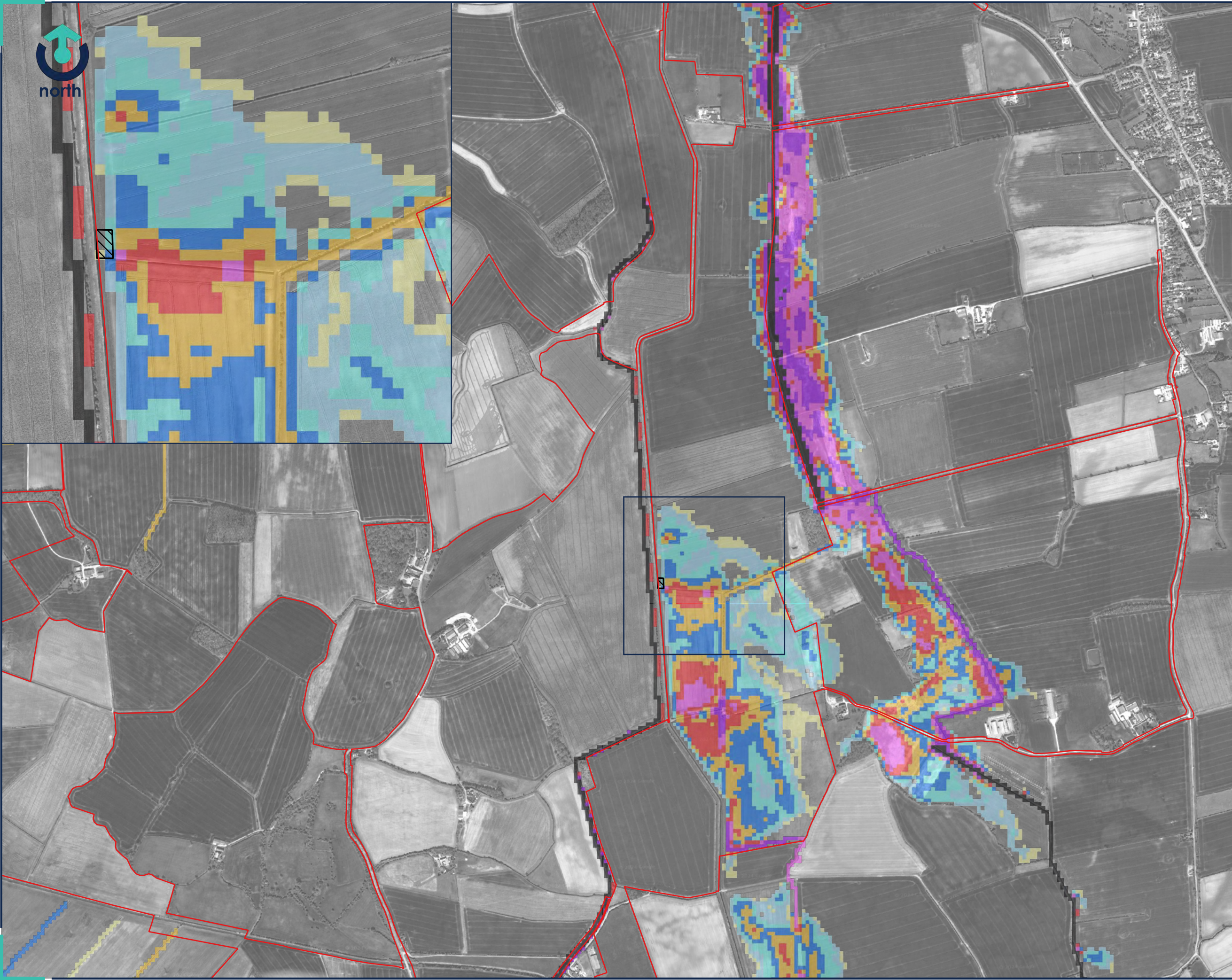
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Monk's Dyke Breach 11
100yr + 17% Maximum Depth



SCALE AT A3: 1:14,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-131	REVISION: -	



Legend

- Site Boundary
- Breach 12
- Depth (m)
- 0 - 0.1
 - 0.1 - 0.3
 - 0.3 - 0.5
 - 0.5 - 0.7
 - 0.7 - 0.9
 - 0.9 - 1.1
 - 1.1 - 1.5
 - 1.5 - 1.8
 - >1.8

-	FIRST ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Monk's Dyke Breach 12
100yr + 17% Maximum Depth












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Legend

- Site Boundary 
- Breach 12 
- Velocity (m/s)
- ≤ 0.25 
 - 0.25 - 0.50 
 - 0.50 - 1.00 
 - 1.00 - 1.50 
 - 1.50 - 2.00 
 - 2.00 - 2.50 
 - > 2.50 

-	FIRST ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

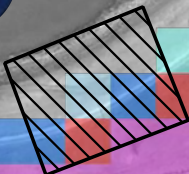
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Monk's Dyke Breach 12
100yr + 17% Maximum Velocity



SCALE AT A3: 1:14,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-134	REVISION: -	



Legend

Site Boundary 

Breach A 

Depths (m)

0 - 0.1 

0.1 - 0.3 

0.3 - 0.5 


0.5 - 0.7 

0.7 - 0.9 

0.9 - 1.1 

1.1 - 1.5 

1.5 - 1.8 

>1.8 

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REV:	DESCRIPTION:	BY:	DATE:

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CLIENT:
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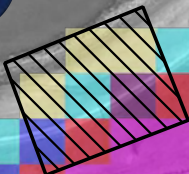
SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach A
100yr + 17% Maximum Depth



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Legend

Site Boundary

Breach A

Velocity (m/s)

<= 0.25	
0.25 - 0.50	
0.50 - 1.00	
1.00 - 1.50	
1.50 - 2.00	
2.00 - 2.50	
> 2.50	

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REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

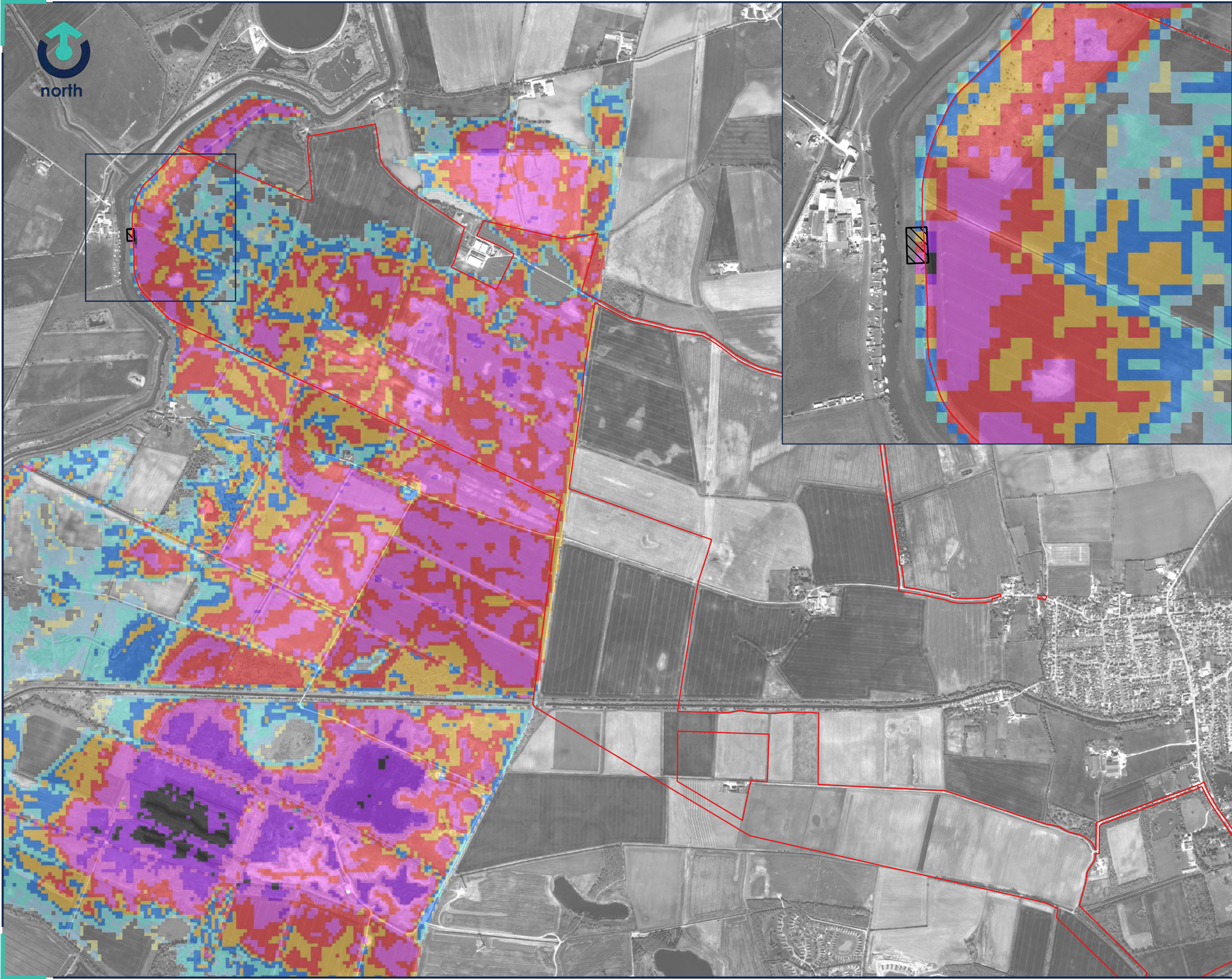
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach A
100yr + 17% Maximum Velocity

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Legend

Site Boundary

Breach B1

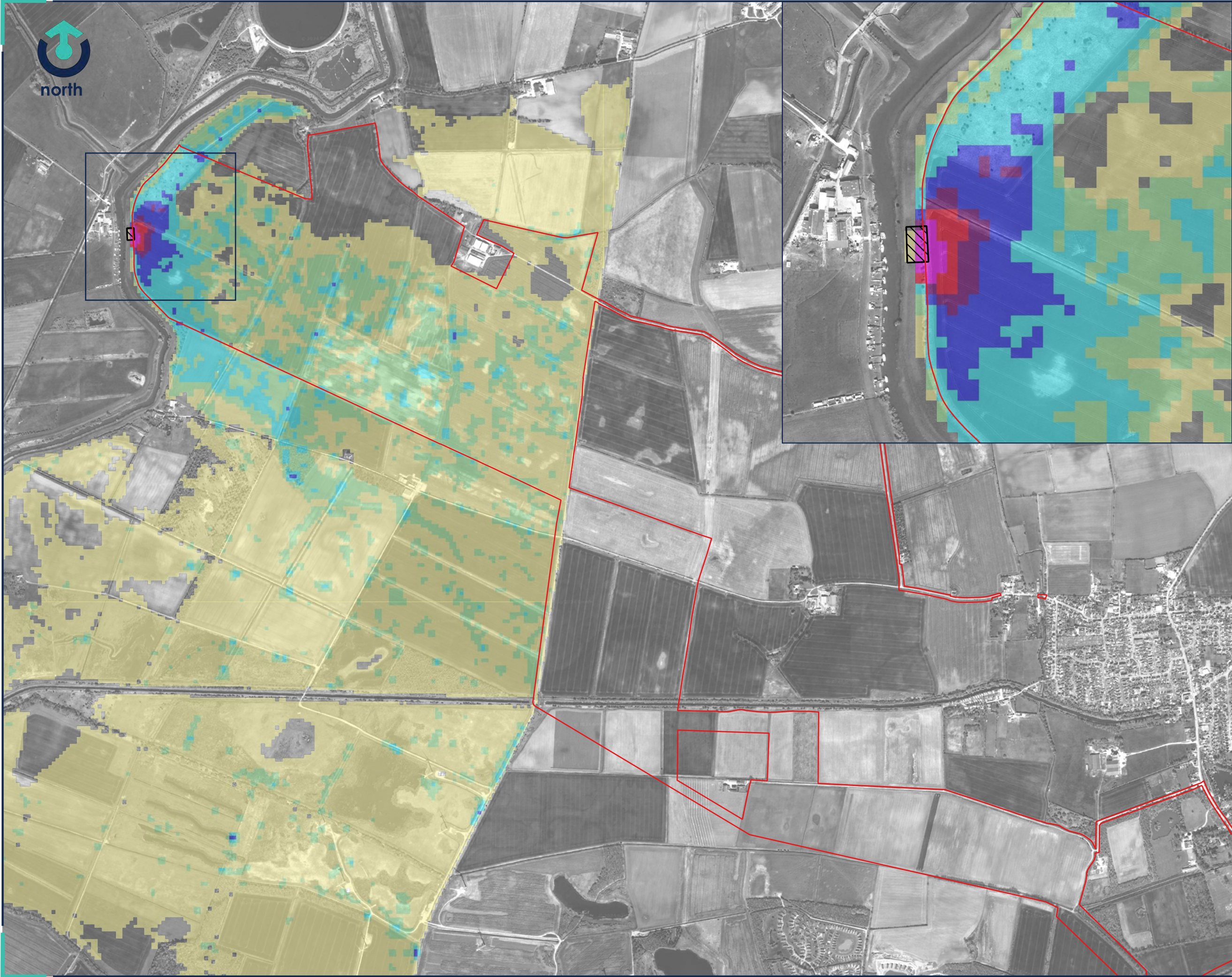
Depth (m)

- 0 - 0.1
- 0.1 - 0.3
- 0.3 - 0.5
- 0.5 - 0.7
- 0.7 - 0.9
- 0.9 - 1.1
- 1.1 - 1.5
- 1.5 - 1.8
- >1.8

01	SECOND ISSUE	CF	24.04.2024
REV:	DESCRIPTION:	BY:	DATE:
STATUS: FOR INFORMATION			
CLIENT: RWE			
SITE: Peartree Hill Solar Farm			
TITLE: Hull River Breach B 100yr + 17% Maximum Depth			


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Legend

- Site Boundary
- Breach B
- Velocity (m/s)
- ≤ 0.25
 - 0.25 - 0.50
 - 0.50 - 1.00
 - 1.00 - 1.50
 - 1.50 - 2.00
 - 2.00 - 2.50
 - > 2.50

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
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SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach B
100yr + 17% Maximum Velocity



SCALE AT A3: 1:15,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-206	REVISION: 01	



Legend

Site Boundary

BREACH D

Depth (m)

- 0 - 0.1
- 0.1 - 0.3
- 0.3 - 0.5
- 0.5 - 0.7
- 0.7 - 0.9
- 0.9 - 1.1
- 1.1 - 1.5
- 1.5 - 1.8
- >1.8

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

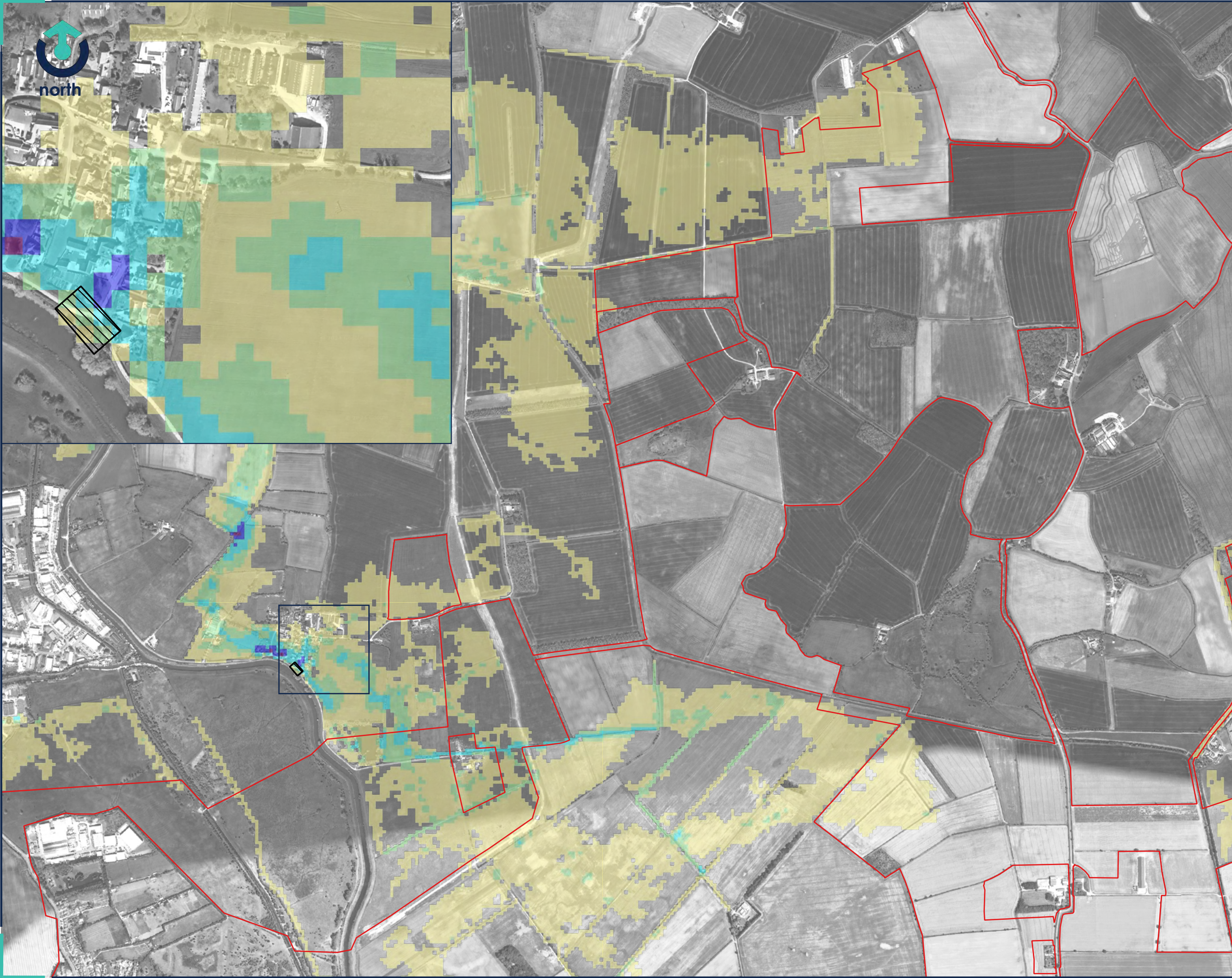
CLIENT:
RWE

SITE:
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TITLE:
Hull River Breach D
100yr + 17% Maximum Depth


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- Legend
- Site Boundary
- BREACH D1
- Velocity (m/s)
- <= 0.25
 - 0.25 - 0.50
 - 0.50 - 1.00
 - 1.00 - 1.50
 - 1.50 - 2.00
 - 2.00 - 2.50
 - > 2.50

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

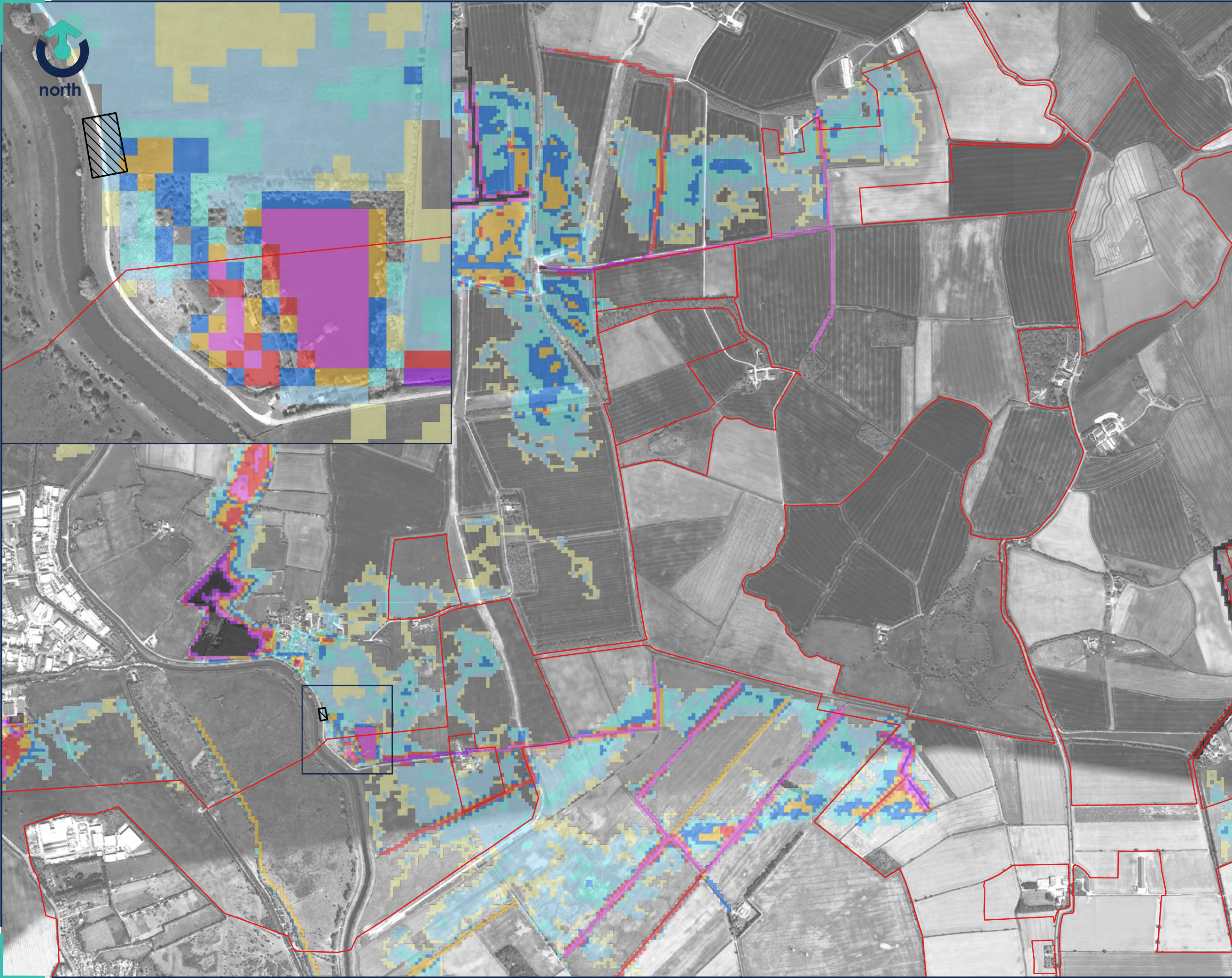
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach D
100yr + 17% Maximum Velocity



SCALE AT A3: 1:15,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-216	REVISION: 01	



Legend

Site Boundary

Breach E1

Depths (m)

- 0 - 0.1
- 0.1 - 0.3
- 0.3 - 0.5
- 0.5 - 0.7
- 0.7 - 0.9
- 0.9 - 1.1
- 1.1 - 1.5
- 1.5 - 1.8
- >1.8

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

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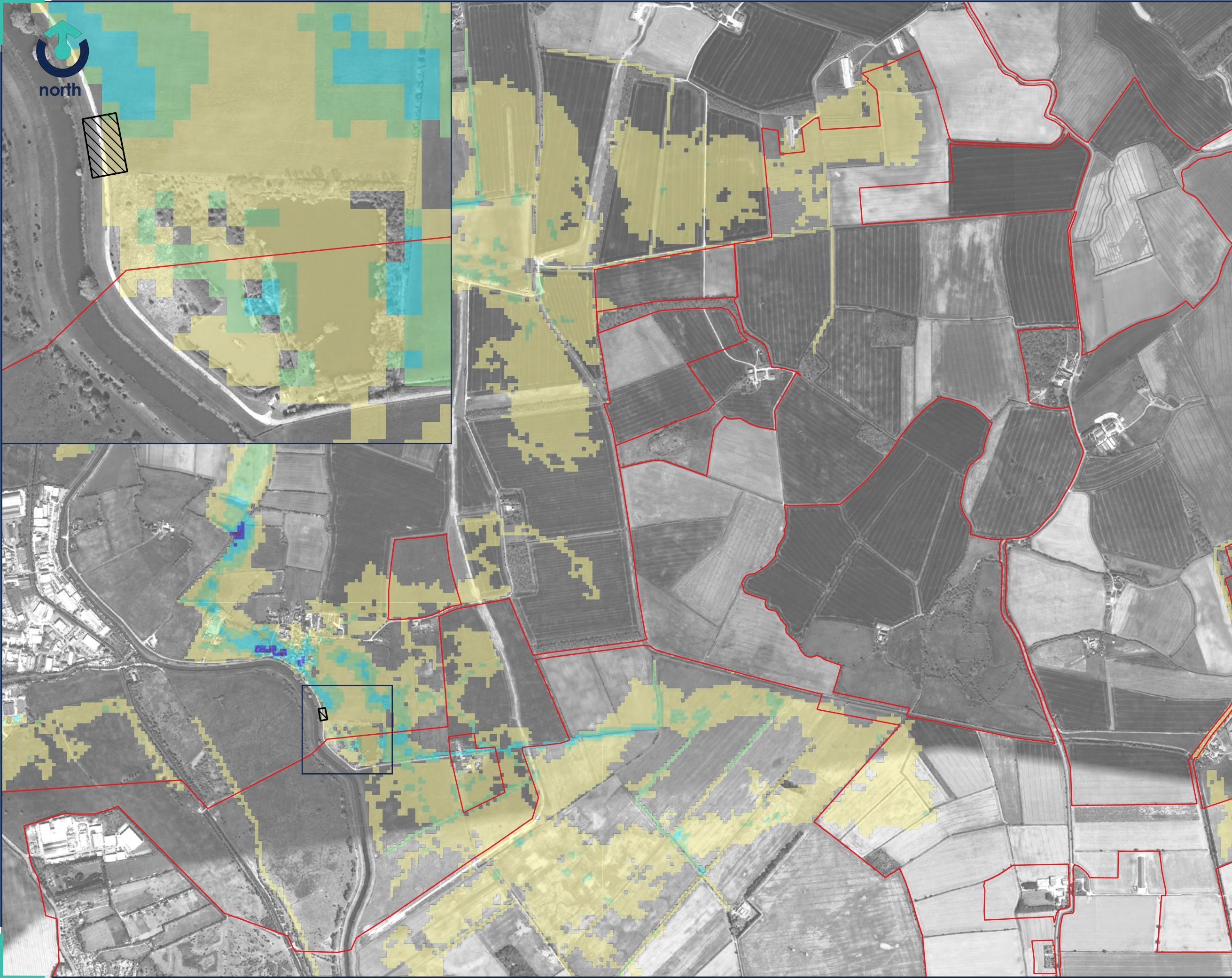
SITE:
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TITLE:
Hull River Breach E
100yr + 17% Maximum Depth

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Legend

Site Boundary

Breach E1

Velocity (m/s)

- <= 0.25
- 0.25 - 0.50
- 0.50 - 1.00
- 1.00 - 1.50
- 1.50 - 2.00
- 2.00 - 2.50
- > 2.50

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

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SITE:

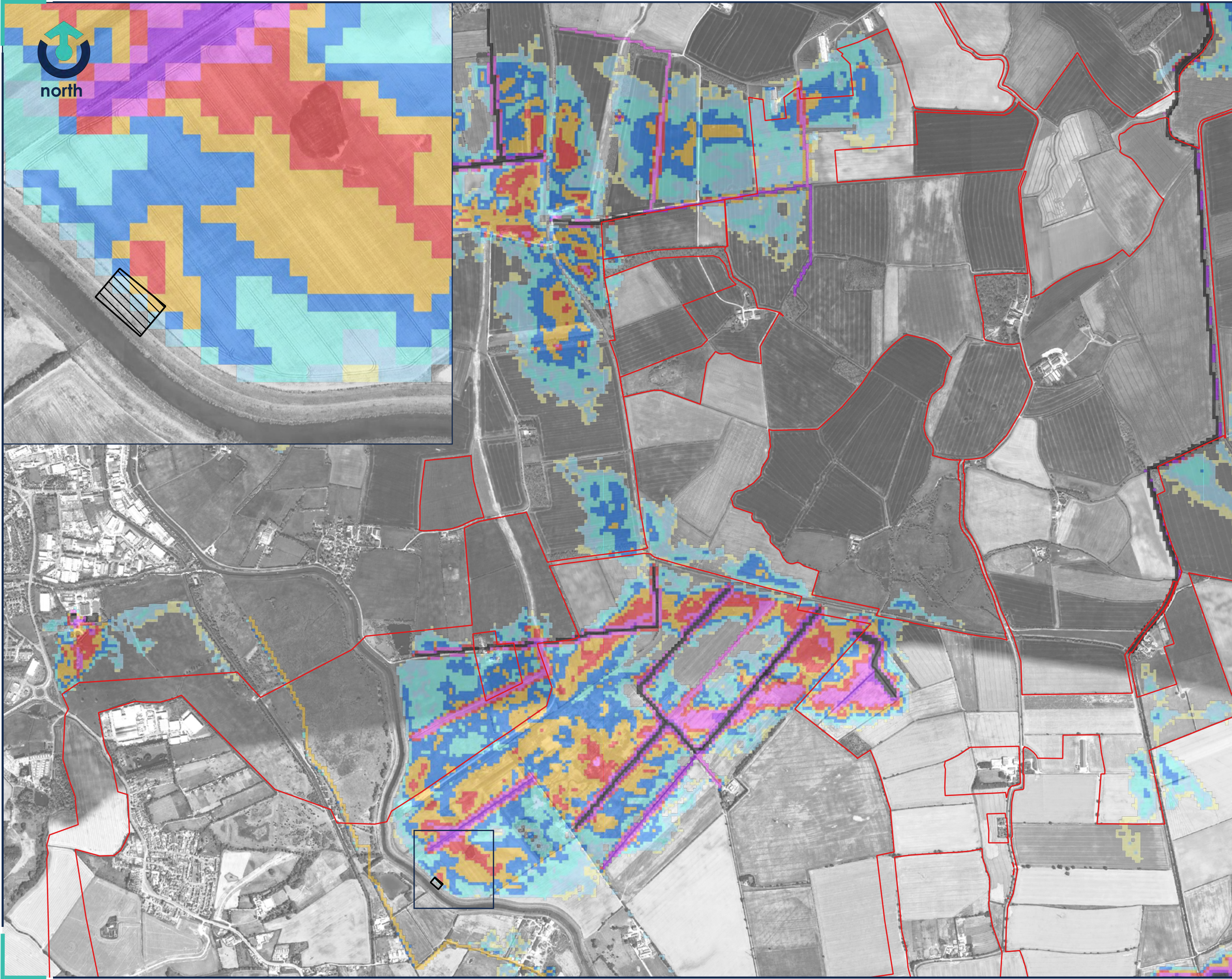
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TITLE:

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100yr + 17% Maximum Velocity

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Legend

- Site Boundary
- Breach F
- Depths (m)
- 0 - 0.1
 - 0.1 - 0.3
 - 0.3 - 0.5
 - 0.5 - 0.7
 - 0.7 - 0.9
 - 0.9 - 1.1
 - 1.1 - 1.5
 - 1.5 - 1.8
 - >1.8

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
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SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach
100yr + 17% Maximum Depth



SCALE AT A3: 1:17,000	DATE: 23.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-221	REVISION: 01	



Legend

Site Boundary

Breach F

Velocity (m/s)
Band 1

- <= 0.25
- 0.25 - 0.50
- 0.50 - 1.00
- 1.00 - 1.50
- 1.50 - 2.00
- 2.00 - 2.50
- > 2.50

01	SECOND ISSUE	CF	23.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

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SITE:

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TITLE:

Hull River Breach
100yr + 17% Maximum Velocity



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PROJECT NO: 20-206	DRAWING NO: 60-222	REVISION: 01	



Legend

Site Boundary 

Breach C 

Depth (m)

0 - 0.1 

0.1 - 0.3 

0.3 - 0.5 

0.5 - 0.7 

0.7 - 0.9 

0.9 - 1.1 

1.1 - 1.5 

1.5 - 1.8 

>1.8 

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REV:	DESCRIPTION:	BY:	DATE:

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SITE:

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TITLE:

Hull River Breach C
100yr + 17% Maximum Depth



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Legend

Site Boundary 

Breach C 

Velocity (m/s)

≤ 0.25 

0.25 - 0.50 

0.50 - 1.00 

1.00 - 1.50 

1.50 - 2.00 

2.00 - 2.50 

> 2.50 

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STATUS: FOR INFORMATION

CLIENT:
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SITE:
Peartree Hill Solar Farm

TITLE:
Hull River Breach C
100yr + 17% Maximum Velocity

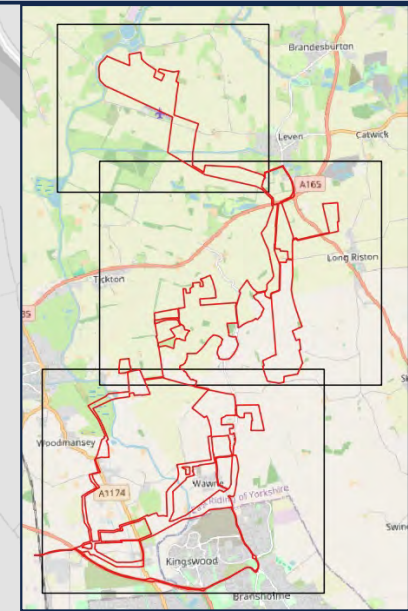


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APPENDIX E

Sensitivity Tests Output Drawings



Legend

Site Boundary

Sensitive Infrastructure

Flood Level Increase (m)

< -0.1

-0.1 to -0.05

-0.05 to -0.01

-0.01 to -0.005

-0.005 to 0.005

0.005 to 0.01

0.01 to 0.05

0.05 to 0.1

> 0.1

Was wet now dry

Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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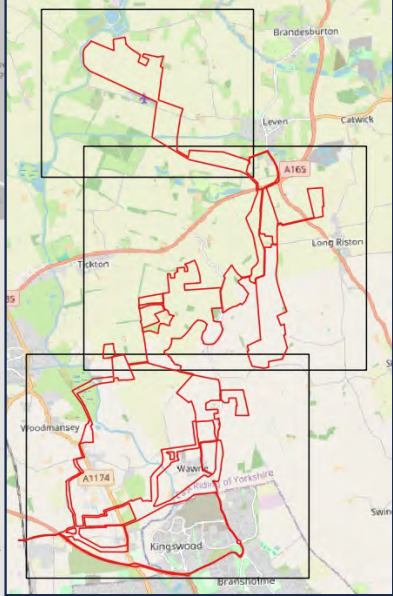
Peartree Hill Solar Farm

TITLE:

Tidal Boundary Sensitivity
Sheet 1 of 3

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PROJECT NO: 20-206	DRAWING NO: 60-231	REVISION: -	



- Legend
- Site Boundary
 - Sensitive Infrastructure
 - Flood Level Increase (m)
 - < -0.1
 - 0.1 to -0.05
 - 0.05 to -0.01
 - 0.01 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.01
 - 0.01 to 0.05
 - 0.05 to 0.1
 - > 0.1
 - Was wet now dry
 - Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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SITE:

Peartree Hill Solar Farm

TITLE:

Tidal Boundary Sensitivity
Sheet 2 of 3



SCALE AT A3: 1:20,000	DATE: 17.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-232	REVISION: -	



Legend

- Site Boundary
- Sensitive Infrastructure
- Flood Level Increase (m)
 - < -0.1
 - 0.1 to -0.05
 - 0.05 to -0.01
 - 0.01 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.01
 - 0.01 to 0.05
 - 0.05 to 0.1
 - > 0.1
- Was wet now dry
- Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	17.04.2024
REV:	DESCRIPTION:	BY:	DATE:

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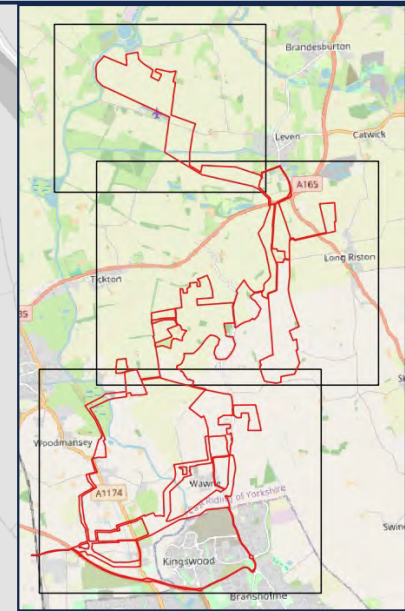
CLIENT:
RWE

SITE:
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TITLE:
Tidal Boundary Sensitivity
Sheet 3 of 3



SCALE AT A3: 1:20,000	DATE: 17.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-233	REVISION: -	



Legend

- Site Boundary
- Sensitive Infrastructure
- Level Increase (m)
 - < -0.25
 - 0.25 to -0.15
 - 0.15 to -0.1
 - 0.1 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.1
 - 0.1 to 0.15
 - 0.15 to 0.25
 - > 0.25
- Was wet now dry
- Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	17.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: INTERNAL USE ONLY

CLIENT:

RWE

SITE:

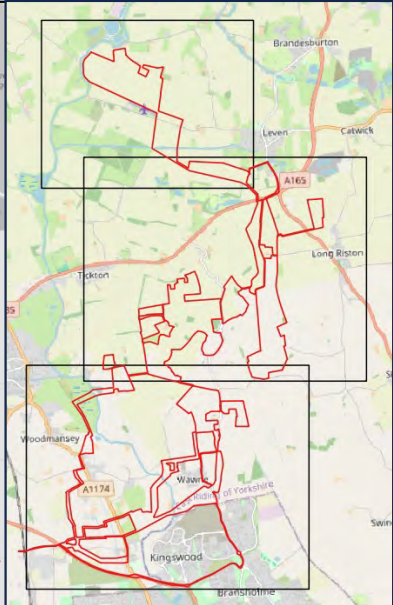
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TITLE:

Flow Sensitivity
Sheet 1 of 3



SCALE AT A3: 1:15,000	DATE: 17.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-234	REVISION: -	



- Legend
- Site Boundary
 - Sensitive Infrastructure
 - Level Increase (m)
 - < -0.25
 - 0.25 to -0.15
 - 0.15 to -0.1
 - 0.1 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.1
 - 0.1 to 0.15
 - 0.15 to 0.25
 - > 0.25
 - Was wet now dry
 - Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	17.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: INTERNAL USE ONLY

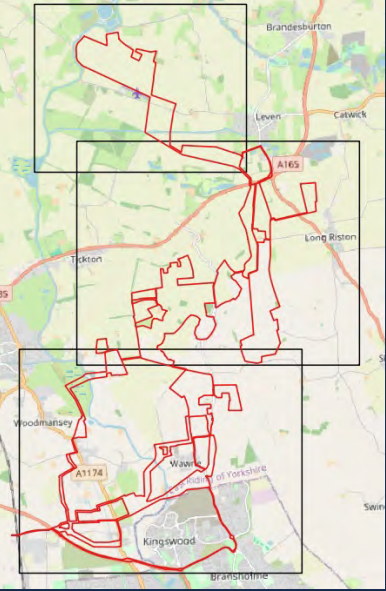
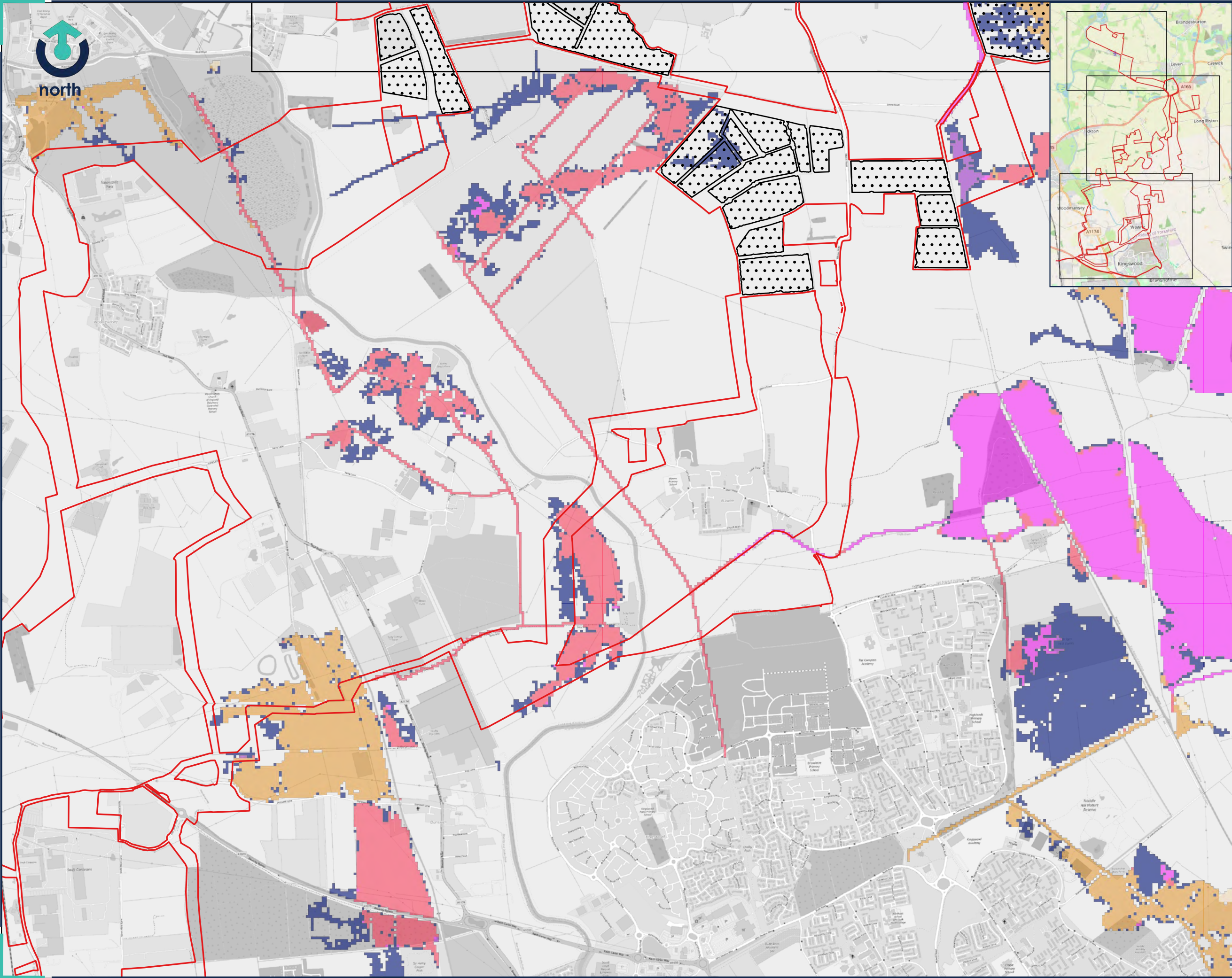
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Flow Sensitivity
Sheet 2 of 3



SCALE AT A3: 1:20,000	DATE: 17.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-235	REVISION: -	



- Legend
- Site Boundary
 - Sensitive Infrastructure
 - Level Increase (m)
 - < -0.25
 - 0.25 to -0.15
 - 0.15 to -0.1
 - 0.1 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.1
 - 0.1 to 0.15
 - 0.15 to 0.25
 - > 0.25
 - Was wet now dry
 - Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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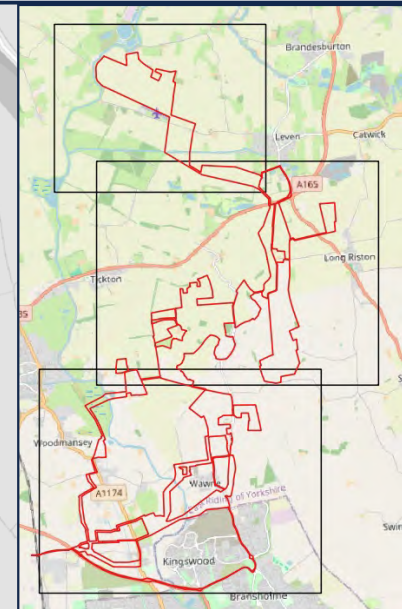
TITLE:
Flow Sensitivity
Sheet 3 of 3



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PROJECT NO: 20-206	DRAWING NO: 60-236	REVISION: -	

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Legend

- Site Boundary
- Sensitive Infrastructure
- Increase (m)
 - < -0.1
 - 0.1 to -0.05
 - 0.05 to -0.01
 - 0.01 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.01
 - 0.01 to 0.05
 - 0.05 to 0.1
 - > 0.1
- Was wet now dry
- Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	18.04.2024
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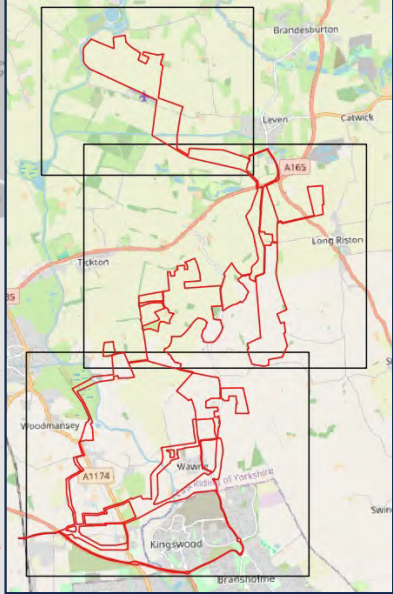
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Manning's Roughness Sensitivity
Sheet 1 of 3



SCALE AT A3: 1:15,000	DATE: 18.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-241	REVISION: -	



- Legend
- Site Boundary
 - Sensitive Infrastructure
 - Increase (m)
 - < -0.1
 - 0.1 to -0.05
 - 0.05 to -0.01
 - 0.01 to -0.005
 - 0.005 to 0.005
 - 0.005 to 0.01
 - 0.01 to 0.05
 - 0.05 to 0.1
 - > 0.1
 - Was wet now dry
 - Was dry now wet

Notes

Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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TITLE:

Manning's Roughness Sensitivity Sheet 2 of 3



SCALE AT A3: 1:20,000	DATE: 18.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-242	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

Increase (m)

< -0.1

-0.1 to -0.05

-0.05 to -0.01

-0.01 to -0.005

-0.005 to 0.005

0.005 to 0.01

0.01 to 0.05

0.05 to 0.1

> 0.1

Was wet now dry

Was dry now wet

Notes

Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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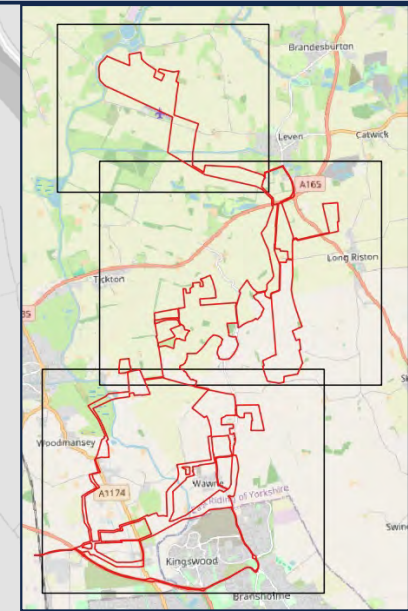
TITLE:

Manning's Roughness Sensitivity Sheet 3 of 3

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PROJECT NO: 20-206	DRAWING NO: 60-243	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

Increase (m)

< -0.1

-0.1 to -0.05

-0.05 to -0.01

-0.01 to -0.005

-0.005 to 0.005

0.005 to 0.01

0.01 to 0.05

0.05 to 0.1

> 0.1

Was wet now dry

Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	18.04.2024
REV:	DESCRIPTION:	BY:	DATE:

STATUS: INTERNAL USE ONLY

CLIENT:

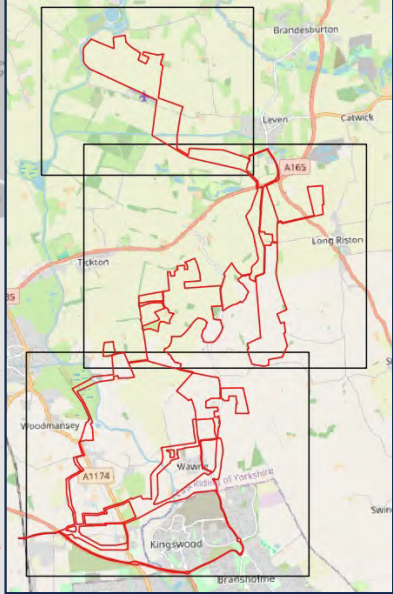
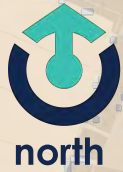
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Developed Areas Roughness Increase Sheet 1 of 3

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PROJECT NO: 20-206	DRAWING NO: 60-244	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

Increase (m)

< -0.1

-0.1 to -0.05

-0.05 to -0.01

-0.01 to -0.005

-0.005 to 0.005

0.005 to 0.01

0.01 to 0.05

0.05 to 0.1

> 0.1

Was wet now dry

Was dry now wet

Notes

Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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SITE:

Pearmtree Hill Solar Farm

TITLE:

Developed Areas Roughness Increase Sheet 2 of 3














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Legend

- Site Boundary 
- Sensitive Infrastructure 
- Increase (m)
- < -0.1 
 - 0.1 to -0.05 
 - 0.05 to -0.01 
 - 0.01 to -0.005 
 - 0.005 to 0.005 
 - 0.005 to 0.01 
 - 0.01 to 0.05 
 - 0.05 to 0.1 
 - > 0.1 
- Was wet now dry 
- Was dry now wet 

Notes

Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	18.04.2024
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STATUS: INTERNAL USE ONLY

CLIENT:

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SITE:

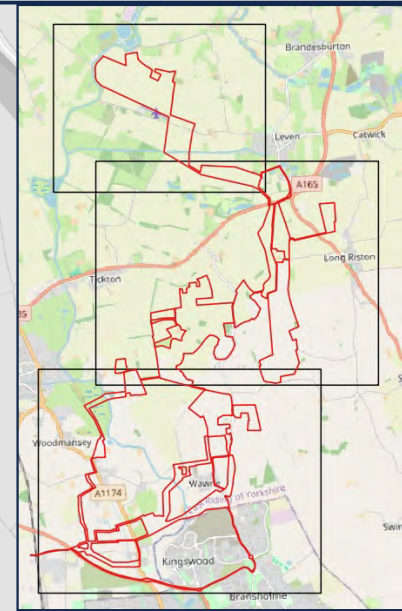
Peartree Hill Solar Farm

TITLE:

Developed Areas Roughness Increase Sheet 3 of 3



SCALE AT A3: 1:20,000	DATE: 18.04.2024	DRAWN: CF	CHECKED: AB
PROJECT NO: 20-206	DRAWING NO: 60-246	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

1D Channel

Level Increase (m)

< -0.2

-0.2 to -0.15

-0.2 to -0.1

-0.1 to -0.005

-0.005 to 0.005

0.005 to 0.1

0.1 to 0.15

0.15 to 0.2

> 0.2

Was wet now dry

Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	23.04.2024
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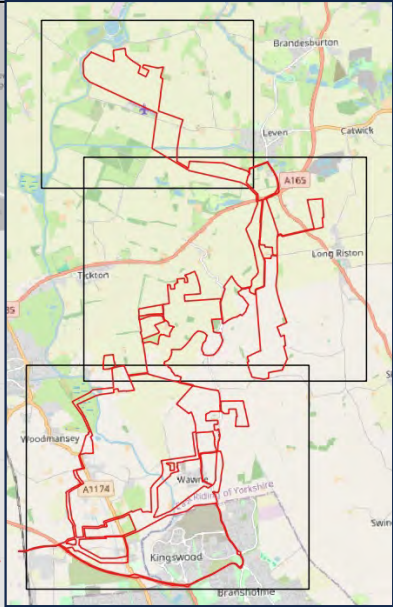
CLIENT:
RWE

SITE:
Peartree Hill Solar Farm

TITLE:
Maximum Credible Scenario
(2100) Level Change Sheet 1 of 3



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PROJECT NO: 20-206	DRAWING NO: 60-247	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

1D Channel

Level Increase (m)

< -0.2

-0.2 to -0.15

-0.2 to -0.1

-0.1 to -0.005

-0.005 to 0.005

0.005 to 0.1

0.1 to 0.15

0.15 to 0.2

> 0.2

Was wet now dry

Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

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STATUS: FOR INFORMATION

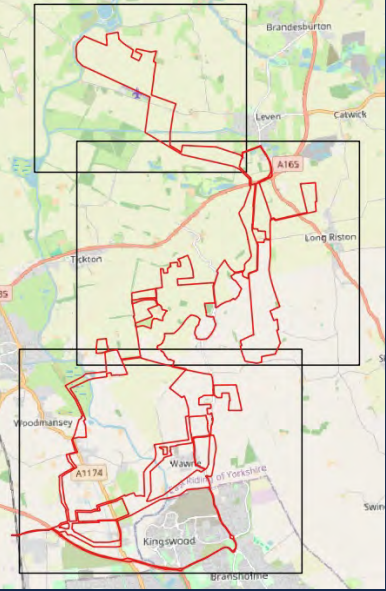
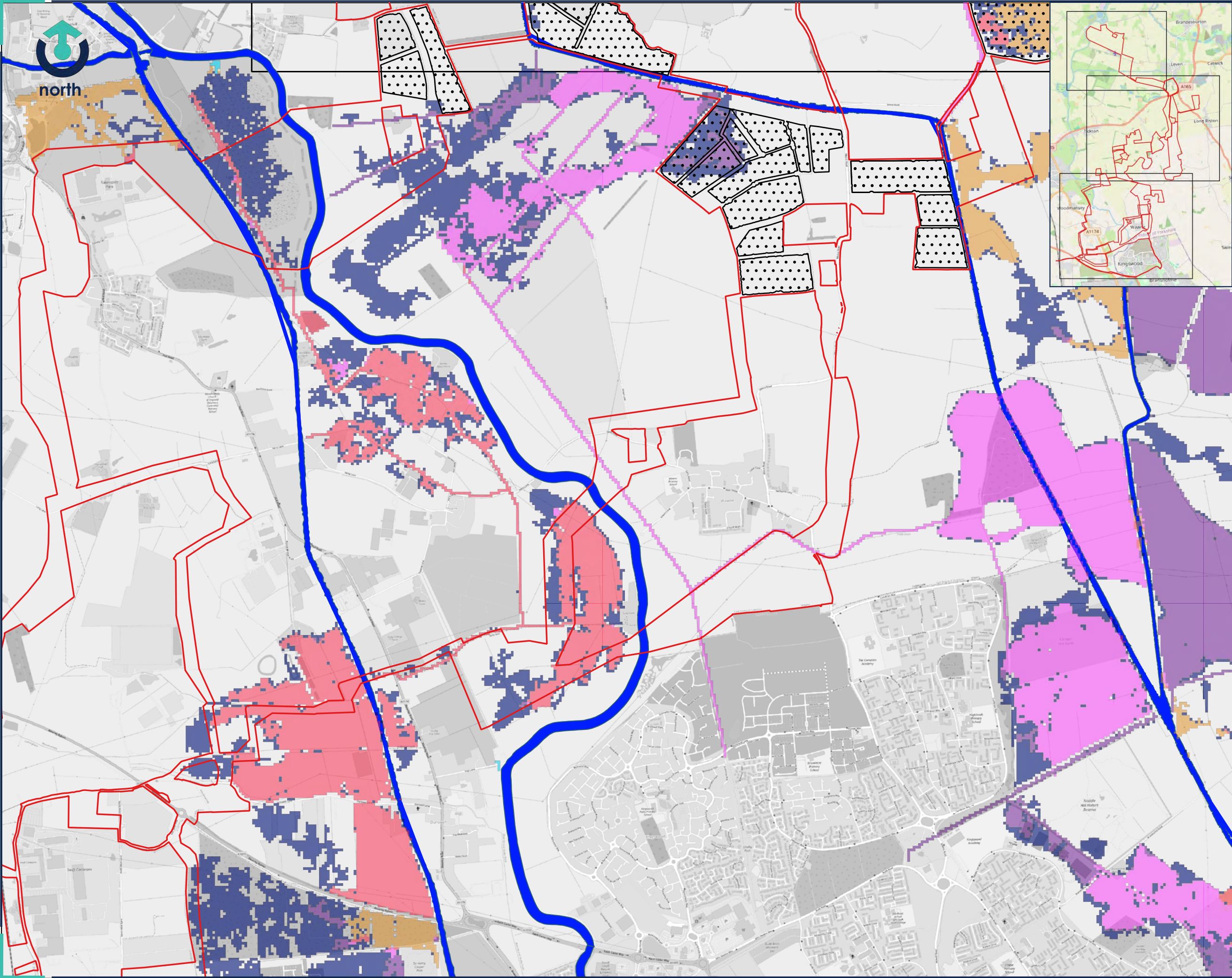
CLIENT:
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SITE:
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TITLE:
Maximum Credible Scenario (2100) Level Change Sheet 2 of 3


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PROJECT NO: 20-206	DRAWING NO: 60-248	REVISION: -	



Legend

Site Boundary

Sensitive Infrastructure

1D Channel

Level Increase (m)
Band 1

< -0.2

-0.2 to -0.15

-0.2 to -0.1

-0.1 to -0.005

-0.005 to 0.005

0.005 to 0.1

0.1 to 0.15

0.15 to 0.2

> 0.2

Was wet now dry

Was dry now wet

Notes
Sensitive infrastructure areas encompass the coverage of solar panels, substations, inverters, battery storage etc. but do not include access or cable routes.

-	FIRST ISSUE	CF	23.04.2024
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STATUS:	FOR INFORMATION
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CLIENT:	RWE
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SITE:	Peartree Hill Solar Farm
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TITLE:	Maximum Credible Scenario (2100) Level Change Sheet 3 of 3
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PROJECT NO: 20-206	DRAWING NO: 60-249	REVISION: -	

APPENDIX F

Hydraulic Modelling Addendum

Title **Hydraulic Modelling Addendum**

Job Name Peartree Hill Solar Farm

Job number 20-206

Date 6th November 2023

1 INTRODUCTION

1.1.1 This Technical Note discusses additional work carried out to support proposed Solar PV development at Peartree Hill following the Environment Agency (EA) review of the development proposals and hydraulic modelling. It forms an addendum to the Peartree Hill Solar Farm Hydraulic Modelling Report 20-206-60-050.

1.1.2 Since submission of Revision 05 of this document to the EA, the development proposals have been updated. The Flood Risk Assessment reflects the updated development proposals.

1.1.3 The modifications were carried out to address comments relating to:

- The potential for maintenance to be withdrawn from defences
- Missing Structures
- The impact of the flow sensitivity runs on vulnerable infrastructure
- Sense checking flood levels against available gauge data.

2 DEFENCES

2.1 EA Comment

2.1.1 The Environment Agency letter dated 25th June 2024 (ref:XA/2024/100093/01-L01) states:

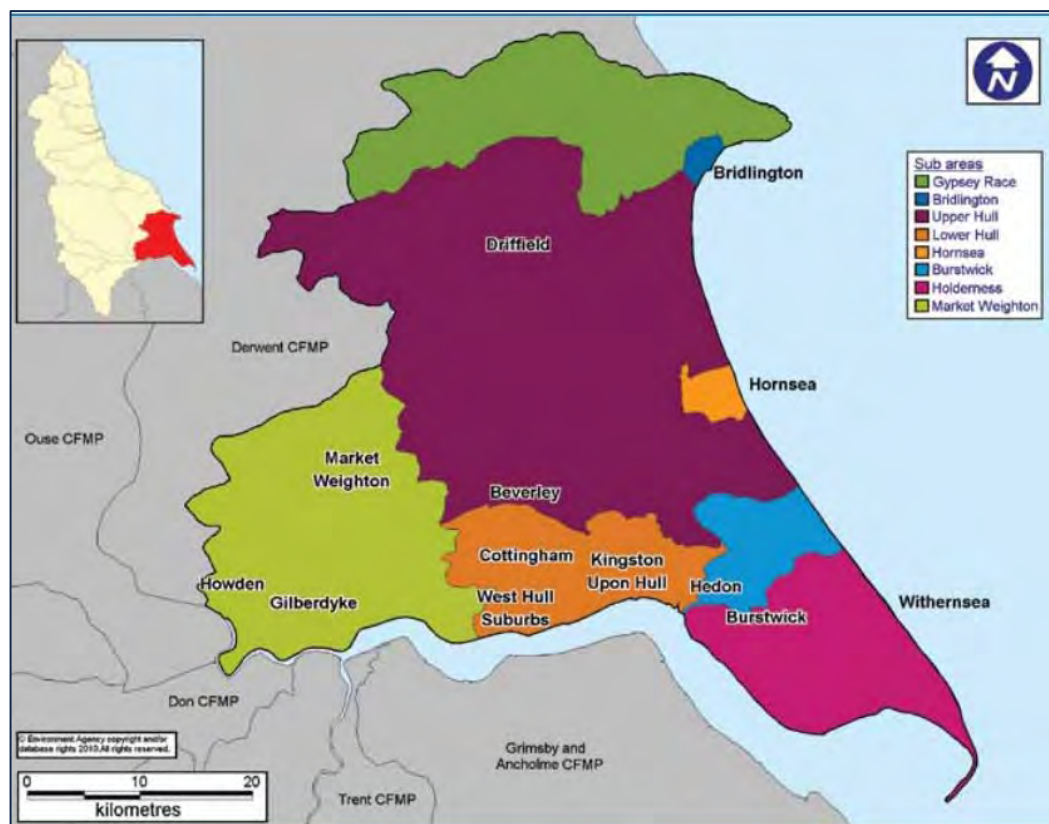
"Although breach modelling is being undertaken by the applicant, any assessment of residual flood risk, both now and in the future, will be insufficient without further consideration of the condition of the flood defences. Through understanding the condition of existing defences and how defence conditions may change over the lifetime of the development, you must give appropriate consideration to how residual flood risk can be managed and mitigated."

2.2 Defences

- 2.2.1 The site benefits from a range of defences. The policy for managing flood risk in this area is set out in the Hull and Coastal Streams Catchment Flood Management Plan (CFMP). The document which was published in 2010 sets out “our preferred plan for sustainable flood risk management over the next 50 to 100 years”.

The defences alongside the Humber Estuary fall within Lower Hull catchment sub-area (as shown in Figure 1-1). The policy for this area is to “take action to further reduce flood risk”.

Figure 1-1 CFMP catchment sub-areas



- 2.2.2 There have recently been significant defence improvements in the area generally consisting of flood embankments and walls which have been designed so a managed adaptive approach can be taken – i.e. so that the height of these defences can be raised in the future to keep pace with sea-level rise should it be required.
- 2.2.3 Give the commitment to defences in this area, the fact that they protect thousands of properties in the City of Hull and that tidal flooding would be significantly attenuated before reaching the site no further investigation is considered necessary, as agreed with the Environment Agency during a meeting on 1st July 2024.

Upper Hull Defences

- 2.2.4 The site and surroundings fall within the Upper Hull subcatchment. The policy for this area is to *"Continue with existing or alternative actions to manage flood risk at the current level"*.
- 2.2.5 The EA cited concerns about the potential for maintenance of the defences to be withdrawn resulting in the defences falling into disrepair.
- 2.2.6 The defences in the Upper Hull subcatchment which afford significant protection to the site are the embankments alongside the River Hull and the Monk Dike. The condition of these defences as recorded in the 'Spatial Flood Defences including Standardised Attributes' data download from data.gov.uk was reviewed and is presented in Drawings 20-206-60-303 & 20-206-60-304 appended to this note.

River Hull Defences

- 2.2.7 The defences on the left bank of the River Hull which afford protection of the site have all been inspected this year (2024) and meet the target condition of 3 categorized as 'Fair'. The River Hull is tidal and significant proportions of land behind it are below high tide levels. Consequently, it is considered extremely unlikely that these defences will be allowed to fall into disrepair over the 40 year lifetime of the development. This create a huge saline/brackish marsh where there is currently significant amount of agricultural land and a number of small settlements.
- 2.2.8 The River Hull embankments adjacent to areas where solar development will be take place (East of Beverley and North of Linley Hill airstrip) are substantial generally 3-4m high and 30-40m wide.
- 2.2.9 Given the condition of these defences, their substantial nature, the policy to maintain them and the widespread effects of withdrawing maintenance no modelling to represent the loss of defences in this area has been carried out.
- 2.2.10 It should be noted however that numerous breach scenarios have been carried out in worst-case locations for the development (with the breach locations and parameters being agreed with the EA). These breaches are instantaneous and are centred around the peak of a future 1 in 100 year fluvial flood event. The loss of large sections of defences in this area would result in flooding being distributed over a wider area and therefore unlikely to exceed the worst-case breach output.
- 2.2.11 It should also be noted that development adjacent to the River Hull (i.e. to the north of Beverley Airfield), has since been removed from the proposals.

Monk Dike Defences

- 2.2.12 The Monk Dike embankments adjacent to proposed solar development were last inspected in 2024. The left (eastern bank) is recorded as meeting it's target condition of 3 – Fair. The northern section of the right (western) bank is in below it's target condition being recorded as 4 – Poor.

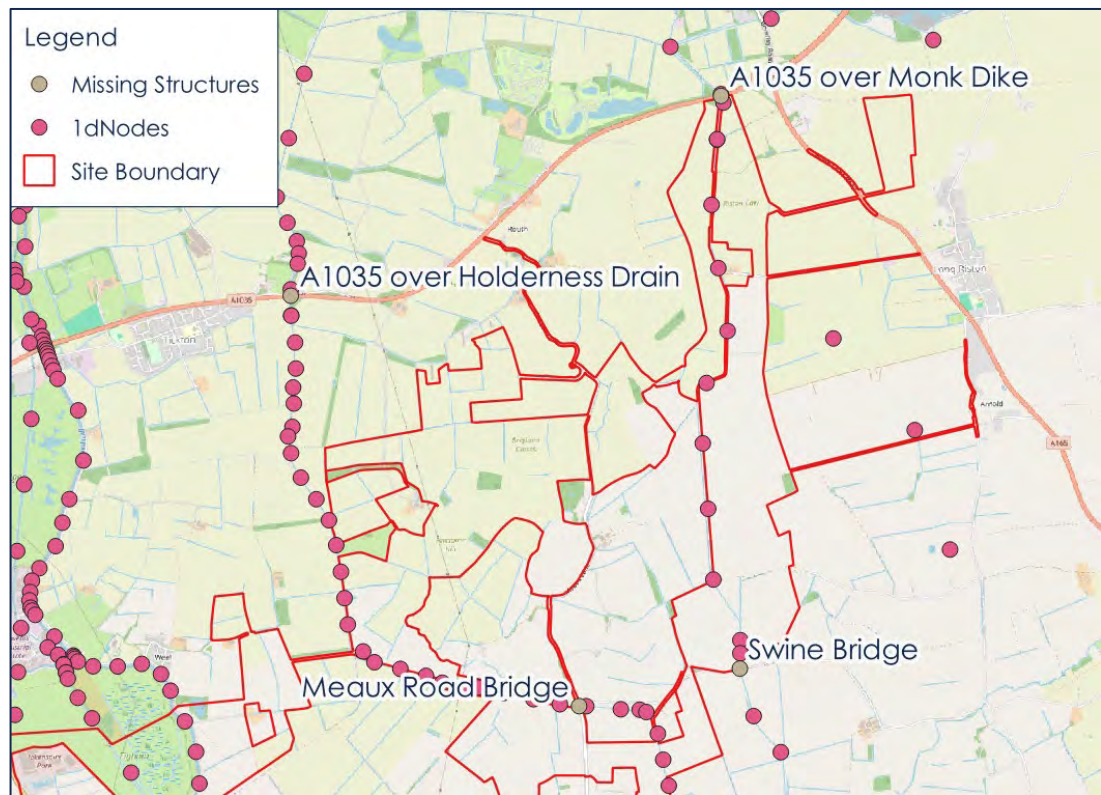
- 2.2.13 A simulation was carried out to determine the impact of complete failure of this defence by adjusting model bank lines to match existing ground levels at the toe of the defence. In essence this represents a situation where the defence is completely removed for its entire reach of approximately 4km.
- 2.2.14 Even if maintenance was withdrawn, it would take a significant period of time for the defence to provide no protection to the site. In fact it is likely that overtopping of the lowest part which is at the northern end of the reach (just south of the A1035) would erode the bank and progressively reduce its height and that further loss of bank would be limited beyond this point.
- 2.2.15 The results of this simulation for the future 1 in 100 year flood is presented in Drawing 20-206-60-253-00 appended to this note. The drawing shows that the extent of flooding on the site only marginally exceeds the maximum breach extent. A review of modelled depths reveals that the flooding is not increased significantly when compared to the combined worst-case from the breach scenarios for the vast majority of the site. The exception being in Parcels B1 & B7 where flood levels are typically 0.1m higher.
- 2.2.16 Although the left (eastern) bank is recorded as being in good condition, there is arguably a larger probability of maintenance being withdrawn (notwithstanding the fact that the solar operator will have significant interest in maintaining the assets to protect their investment) than there is for the River Hull.
- 2.2.17 As the Monk Dike preferentially overtops the low spot in the right bank at the upstream end of the site, the more likely mechanism for failure of the left bank would be seepage, piping and then collapse of a section of the bank. For this reason, to assess the potential impact of this a section of the bank was removed where ground levels at the toe are the lowest. This will produce a similar result as removing the entire reach as ground levels elsewhere are higher and overtopping is unlikely to occur.
- 2.2.18 The results of this simulation for the future 1 in 100 year flood is presented in Drawing 20-206-60-253-00 appended to this note. The extent of flooding adjacent to the section of defence removed is almost identical to the worst-case breach scenario and flood levels are just 5mm higher.

3 MISSING STRUCTURES

- 3.1.1 The EA model review notes a number of missing structure in vicinity of the site as listed below and shown in Figure 3-1:
- A1035 bridge over Monk Dike (FM cross section Cat00000)
 - A1035 bridge over Holderness Drain (FM cross section HN43),
 - Swine Road Bridge over Monk Dike (closest FM cross section MK4055), and
 - Meaux Road Bridge over Holderness Drain (FM cross section HN21).

- 3.1.2 Three of these structures have been added to the model using available data and where information was sparse a conservative approach to the structure definition was taken. The structure at HN21 as it appears to be a clear span structure with the deck approximately 3m above the maximum water level. Structure details definitions are appended to this document.

Figure 3-1 Missing Structures



- 3.1.3 The model was reran with the design event flood. The maximum flood level was compared with the existing baseline design event outputs and the results are shown in Drawing 20-206-60-255-00 & 20-206-60-256-00.
- 3.1.4 Flood levels are generally within +/-20mm within the site boundary, the exception being a small part of parcel B1 where levels are reduced by 60mm and land west of parcel F12 where levels are reduced by 180mm. The only significant increase within the site are the parcels to the east of the Monk Dike (B2-4, B8 & C1-C3) where levels increase by 20mm. The change in outline is insignificant.
- 3.1.5 Given the very minor changes experienced in flood levels across the site it is concluded that the definition of these structures has no material impact on the flood levels, the mitigation (a freeboard of 300mm has been applied), or the layout.
- 3.1.6 As an additional sensitivity the bridge openings were reduced as follows:
- Cat0000 – from 6m to 4m wide
 - MK3935 – from 5.5m to 4m wide
 - HN43 – from 3.5m wide to 2.5m wide

4 IMPACT OF FLOW SENSITIVITY ON VULNERABLE INFRASTRUCTURE

4.1.1 The EA letter pertaining to the review of the hydraulic modelling (ref: XA/2024/100110/01-L01) includes the following query.

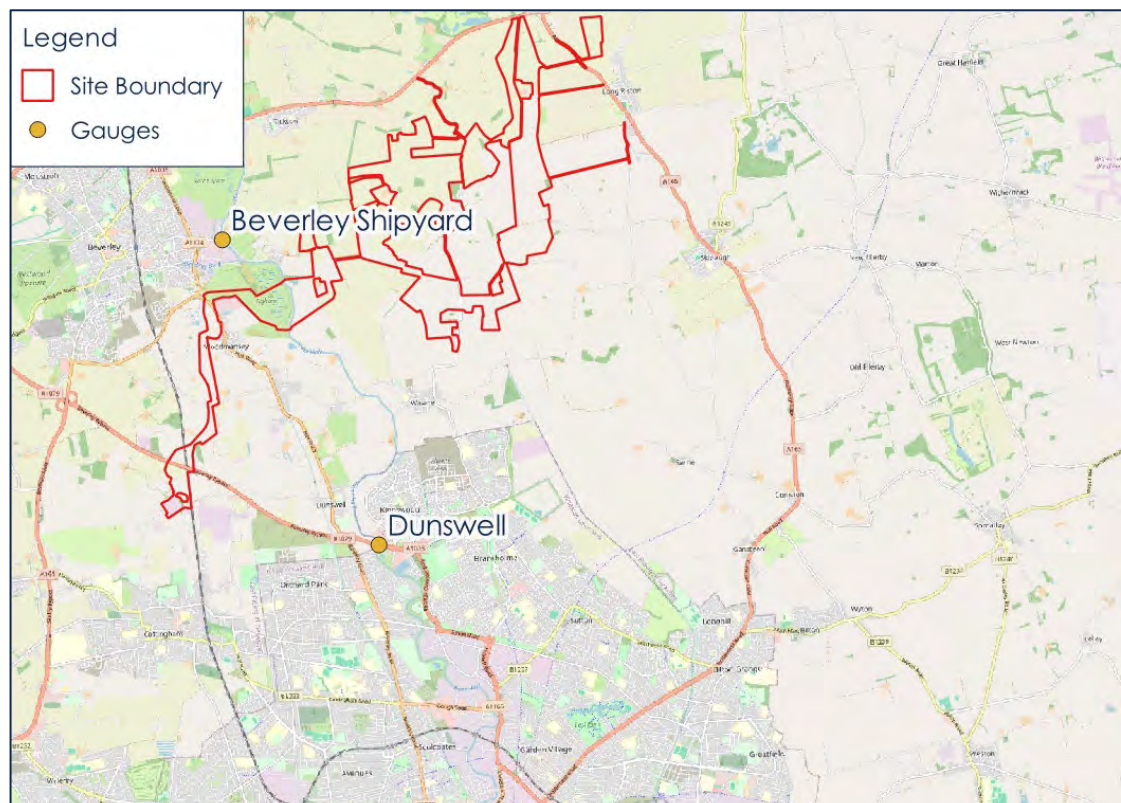
"There are some areas of additional flooding in the baseflow/SPR sensitivity test within the development area. Is sensitive infrastructure located outside of these areas?"

4.1.2 There is no sensitive infrastructure in these areas. Solar panels will be in these areas but will be raised significantly above the predicted flood levels. A revised version of the flow sensitivity drawings which includes containerised infrastructure and substation locations is appended to this note.

5 GAUGE LEVELS CHECK

The EA model review spreadsheet includes peak water levels for most years for two gauges: Dunswell gauge starting from 2001 and the Beverley Shipyard gauge starting from 1994. The location of the gauges is shown in Figure 4-1.

Figure 4-1 Gauge Locations.



5.1.1 Both of these gauges are located on the River Hull which is heavily tidally influenced and drains a large catchment so the causes of high levels are difficult to apportion. This is complicated by the fact the tidal ingress and fluvial egress are prevented when the Hull Tidal Surge barrier is closed.

- 5.1.2 The levels at Beverly Shipyard which are most relevant for the site vary between 2.99mAOD and 3.89mAOD over the 29 year record and have an average value of 3.54mAOD. When accounting for the predicted sea level rise to 2066 of 0.36m, the peak modelled flood level of 4.06mAOD seems reasonable.
- 5.1.3 The tidal boundary has been subject to sensitivity testing as have the fluvial flows neither of which produce significantly different results.

Enclosures

Revised Site Layout

Structure Information

20-206-60-303-00 Inland Defences (Sheet 1 of 2)

20-206-60-304-00 Inland Defences (Sheet 2 of 2)

20-206-60-253-00 Monk Dike Defence Removal West – 1 in 100yr +17% Depths

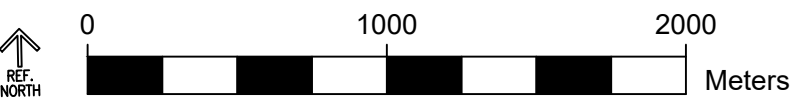
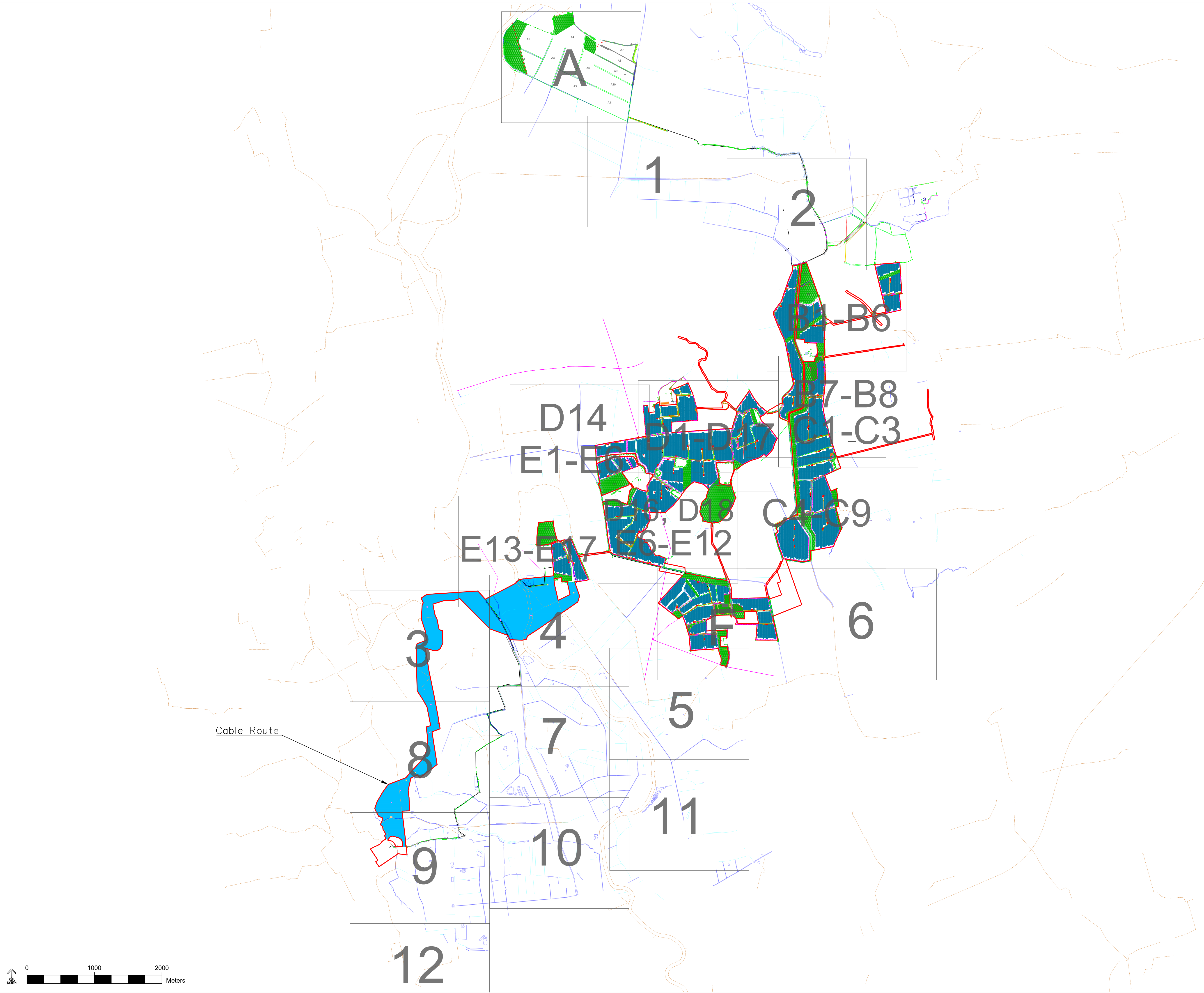
20-206-60-254-00 Monk Dike Defence Removal East – 1 in 100yr +17% Depths

20-206-60-255-00 Structure Sensitivity 1 in 100 yr Flood Level Changes (Sheet 1 of 2)

20-206-60-256-00 Structure Sensitivity 1 in 100 yr Flood Level Changes (Sheet 2 of 2)

20-206-60-235-01 Flow Sensitivity (Sheet 1 of 2)

20-206-60-236-01 Flow Sensitivity (Sheet 2 of 2)



NOTES

- 1. All details are indicative only.
- 2. Dimensions are in metres unless stated otherwise.
- 3. Refer to HSE document "Avoiding danger from overhead power lines – Guidance Note GS6" to ensure safe operation of machinery in proximity to overhead power lines.
- 4. Contains OS Data © Crown copyright and database rights 2023 Ordnance Survey 0100031673
- 5. CCTV Icons are indicative positions at 1.5m from the fence line

LEGEND

- Planning Red Line
- Landowners Line
- Road
- Landowner Road
- Solar panels
- Fence
- Hedges
- Trees
- Hybrid Inverter Container
- Spares Container Container
- Customer Switch Gear Container
- CCTV
- Access Gate
- Construction compound
- Substation Construction Compound
- Drains
- River
- Bank
- Public Rights Of Way
- Proposed Permissive Path
- Proposed Permissive path (allowing travel on horses)
- Gas Pipe
- Water Pipe
- Fuel Pipe
- High Voltage Cable
- Low Voltage Cable
- Telecom Cable
- Wind Turbine
- Acoustic Fencing
- DNO Operational Land
- Wildlife Enhancement
- Archaeological Buffers
- Hedge Punch through/ Culvert Crossing/ Cable Direction Drill



DETAILS	
TITLE	Peartree Hill Solar
LOCATION	Near Drove Lane, Wawne, East Riding of Yorkshire, England, HU7 5XZ, United Kingdom.
DATE	August 24
CONFIGURATION	Typical fixed design
REVISION	6

1 A1035 BRIDGE OVER MONK DIKE

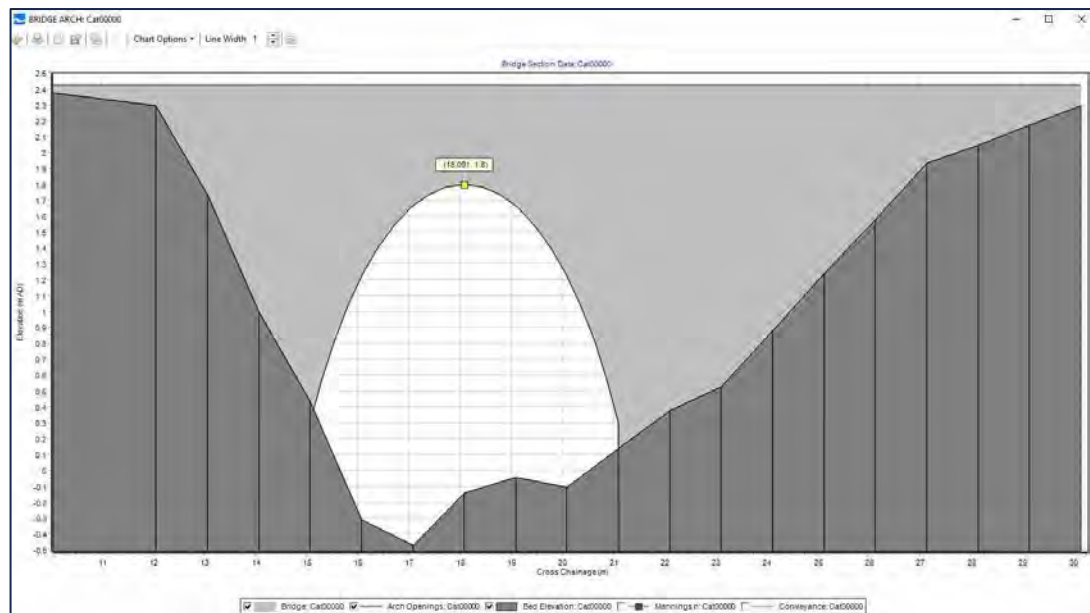
- 1.1.1 The arch bridge where the A1035 crosses the Monk Dike is located between node Cat00000 and Mk8550. The deck level is approximately 3.1mAOD.



1.1.2 The bridge dimensions were estimated with reference to the photos above and assumed brick dimensions of 225mm long, 113mm wide and 75mm high with and additional 10mm allowance for mortar. The parapet capping beam was assumed to be 225mm.

- The parapet was calculated to be 4.2mAOD. 1.1m high – ten course of bricks and capping beam $(85*10+225)/1000$
- The crown was calculated to be 1.8mAOD. 2.35m below parapet – two bricks lengthwise, one width wide, 18 courses and a capping beam $(2*(225+10)+113+18*(75+10)+225)/1000$
- Springing height was calculated to be 0.3mAOD. 1.5m below crown 18 courses plus mortar $18*85/1000$.
- The width of the bridge was estimated to be 6.1m, 26 lengths plus mortar $(225+10)*26/1000$.

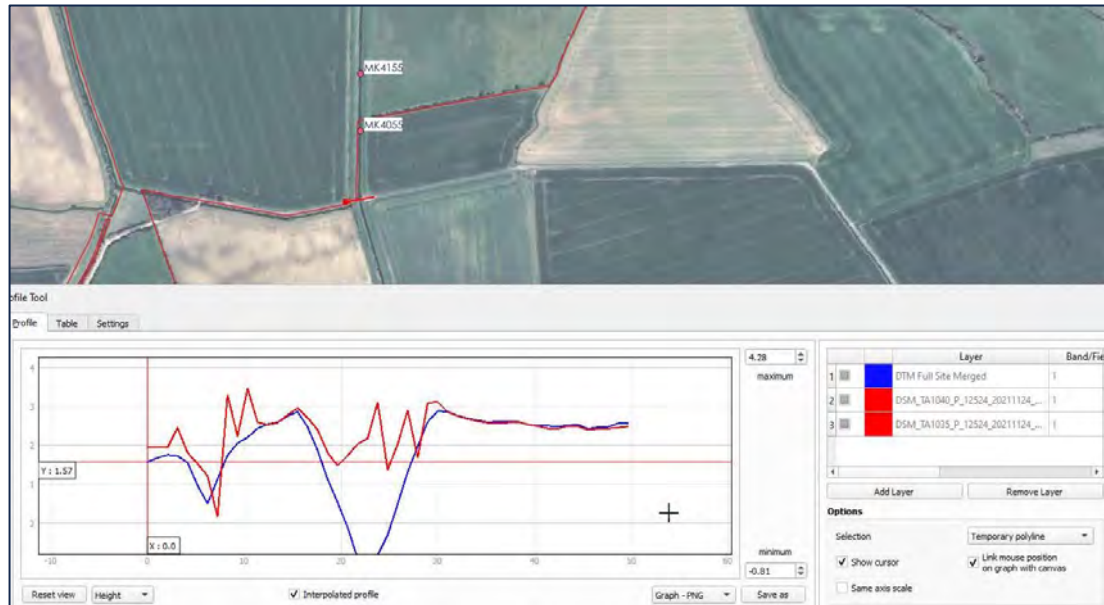
1.1.3 The model definition of the bridge is shown below.



1.1.4 The change to the model results in a reduction in peak flood level in the Monk Dike of 8mm. There is a minor reduction in flooding to the west of Monk Dike and minor increase in flood levels to east of Monk Dike (refer to Drawing 20-206-60-255).

2 SWINE ROAD BRIDGE OVER MONK DIKE

2.1.1 Swine Bridge is located between model nodes MK4055 and MK4355 just beyond the southern edge of parcel C7. The deck level is recorded by LiDAR as being approximately 3mAOD as shown below.



2.1.2 The structure dimensions were estimated from the photograph shown below.

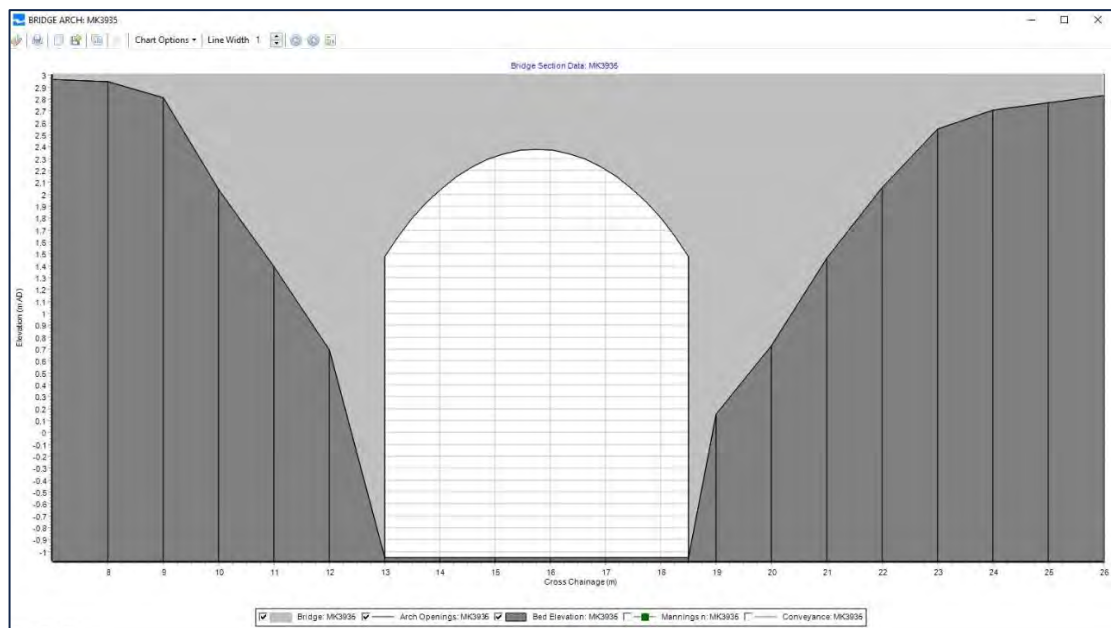


2.1.3 The bridge dimensions were estimated with reference to the photos above and assumed brick dimensions of 225mm long, 113mm wide and 75mm high with and additional 10mm allowance for mortar. The parapet capping beam was assumed to be 225mm.

- The parapet was calculated to be 4.1mAOD. 1.1m high – ten course of bricks and capping beam ($85 \times 10 + 225 / 1000$)

- The crown was calculated to be 2.4mAOD. 1.7m below parapet – two bricks lengthwise, one width wide, 10 courses and a capping beam $(2*(225+10)+113+18*(75+10)+225)/1000$
- Springing height was calculated to be 1.5mAOD. 0.9m below crown 11 courses plus mortar $(11*85/1000)$.
- The width of the bridge was estimated to be 5.6m, 24 lengths plus mortar $24*(225+10)/1000$.

2.1.4 The model definition of the bridge is shown below.



The peak flood level upstream of the bridge is within 1mm of the baseline model and consequently the definition of this bridge is not considered to be significant.

3 A1035 TICKTON BRIDGE OVER HOLDERNESS DRAIN

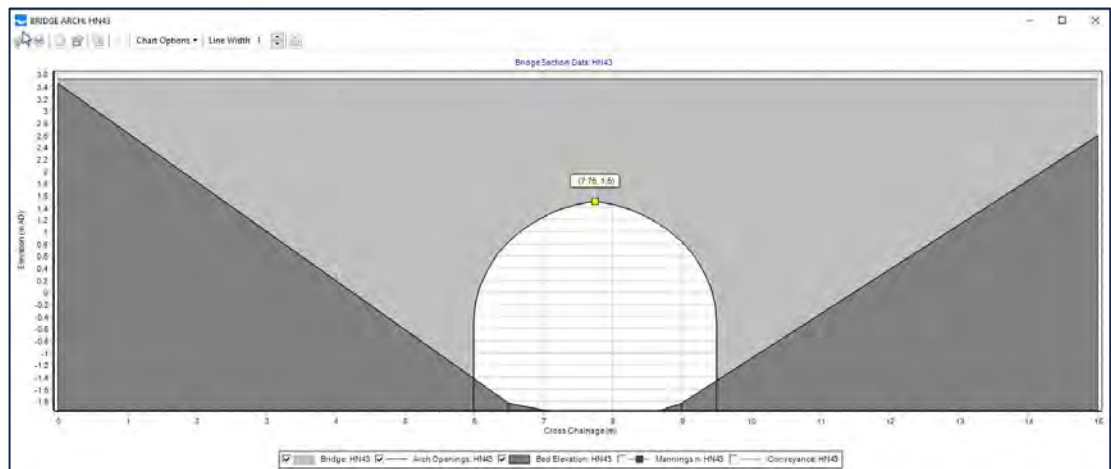
- 3.1.1 Tickton Bridge is located between model nodes HN43 and HN42. It is upstream of the application site. The deck level as recorded by LiDAR data is approximately 3.25m as shown below.



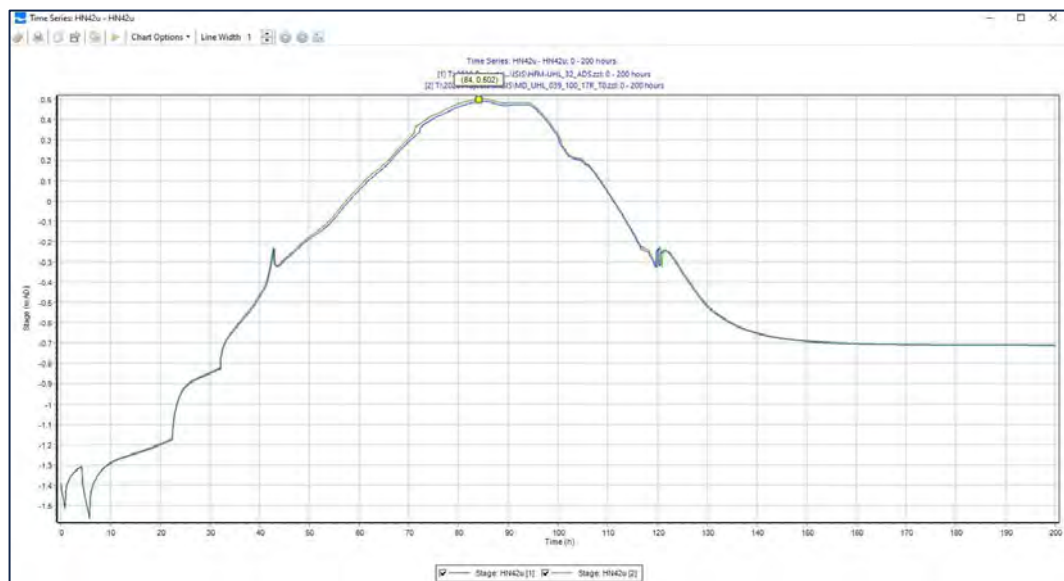
3.1.2 The only available information for the bridge is a photograph provided by the EA shown below.



3.1.3 It was estimated that the bridge opening is 3.5m wide with a 2m high arch and a total structure height of 3m as shown below.



- 3.1.4 The addition of the bridge results in an 11mm increase in water level just downstream of the structure as shown below and a negligible change in flood outline (refer to Drawing 20-206-60-255).

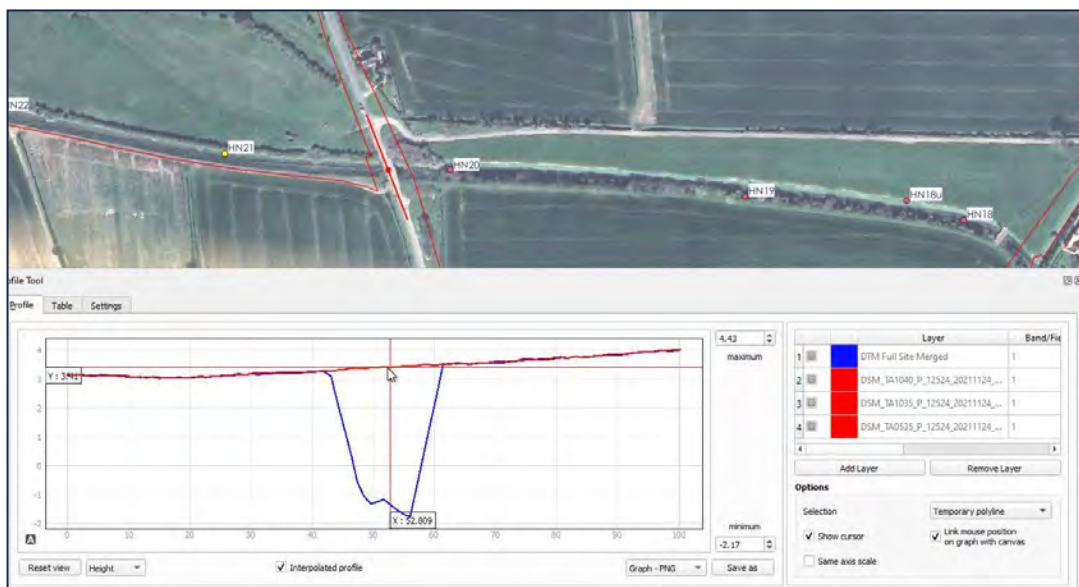


4 HN21

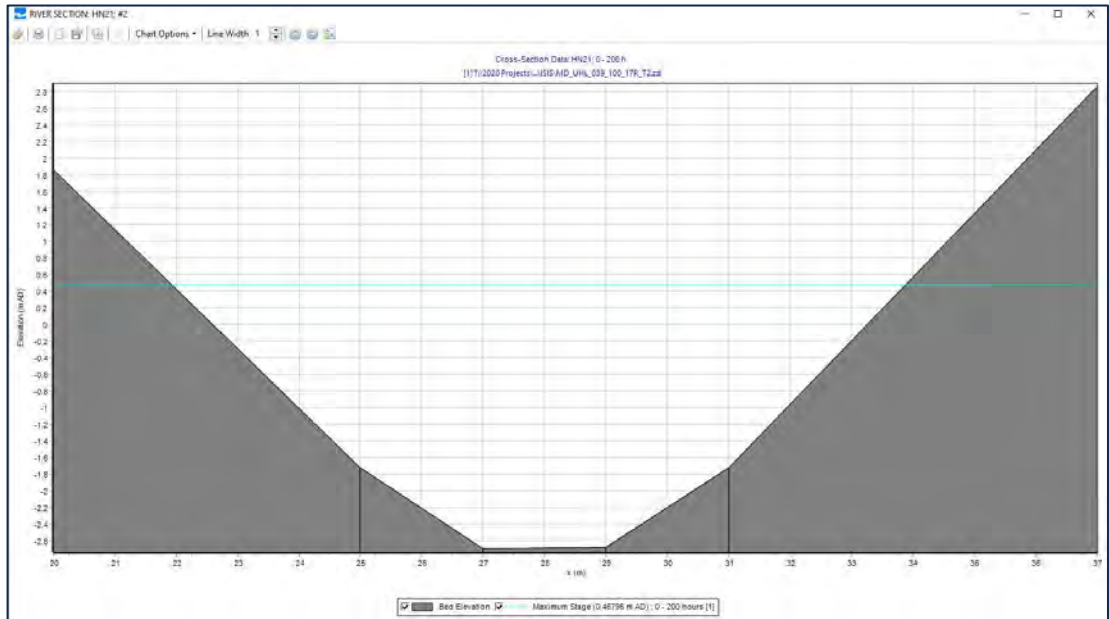
- 4.1.1 There is no bridge in the model between nodes HN21 and HN22 which is located adjacent to Parcel F6. The structure appears to be a flat deck, clear-span bridge as shown below



4.1.2 LiDAR data reports the bridge deck to be 3.25-3.5mAOD as shown below.



4.1.3 The maximum water level during the design event flood at node HN21 just upstream of the structure is 0.5mAOD as shown below. Consequently the soffit is likely to be much higher than the peak water level. The structure would therefore not impede flow and has not been added to the model.





Legend

- Site Boundary
- Defences
 - Very Poor
 - Poor
 - Fair
 - Good
 - Very Good
 - Unchecked
 - No Data

-	FOR INFORMATION	AB	23.07.24
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
RWE

SITE: Peartree Hill Solar Farm
TITLE: Inland Defences (1 of 2)



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PROJECT NO: 20-206	DRAWING NO: 60-303	REVISION: -	



Legend

- Site Boundary
- Defences
 - Very Poor
 - Poor
 - Fair
 - Good
 - Very Good
 - Unchecked
 - No Data

-	FOR INFORMATION	AB	23.07.24
REV:	DESCRIPTION:	BY:	DATE:

STATUS: FOR INFORMATION

CLIENT:
RWE

SITE: Peartree Hill Solar Farm
TITLE: Inland Defences (2 of 2)



SCALE AT A3: 1:30,000	DATE: 23.07.24	DRAWN: AB	CHECKED: PG
PROJECT NO: 20-206	DRAWING NO: 60-304	REVISION: -	